

## Lean NO<sub>x</sub> Catalysis over Sn/γ-Al<sub>2</sub>O<sub>3</sub> Catalysts

M. C. Kung, P. W. Park, D.-W. Kim, 1 and H. H. Kung<sup>2</sup>

Department of Chemical Engineering, Northwestern University, Evanston, Illinois 60208-3120

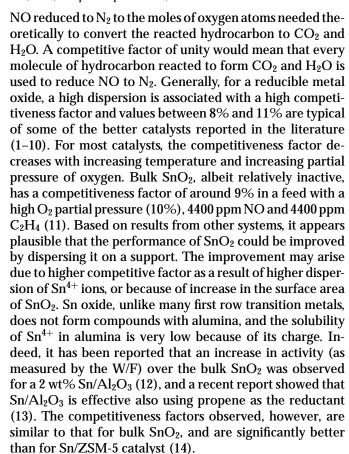
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Sn/y-Al<sub>2</sub>O<sub>3</sub> were effective and highly stable catalysts for NO reduction with propene under high partial pressures of oxygen and water. The activity depended on the Sn loading. For a 10 wt%  $Sn/Al_2O_3$  at 475–500°C, 58% conversion of 1000 ppm NO to  $N_2$ was obtained in the presence of 10% water and 15% O2, at a space velocity of 30,000  $h^{-1}$ , and 77% conversion at 15,000  $h^{-1}$ . The NO conversion increased with O<sub>2</sub> partial pressure but was suppressed by water below 500°C. The activity was also suppressed by SO<sub>2</sub> but could be restored slowly after the removal of SO<sub>2</sub>. © 1999 Academic Press

The increasingly stringent government regulations on the emission level of nitrogen oxides from transportation vehicles resulted in the recent intense research in the area of catalytic reduction of  $NO_x$  to  $N_2$  with hydrocarbons. This is particularly so for emissions from diesel engines which cannot be treated effectively with the highly developed three-way catalysts. For such an application, a practical catalyst needs to be effective in the presence of about 10% oxygen and 10% water vapor, a condition that precludes the use of most of the metal-ion exchanged zeolite catalysts reported to date as it causes the destruction of the zeolite structure and limits the life-time of the cata-

Metal oxides supported on alumina have also been investigated for NO<sub>x</sub> reduction under these conditions. It has been found that, among different variables, the effectiveness of these catalysts for NO<sub>x</sub> reduction depends on the state of the metal oxide on the alumina, which in turn depends on the loading of the metal oxide, the calcination temperature, and the source of alumina. This has been shown recently for  $Ag/Al_2O_3$  (3–5),  $Au/Al_2O_3$  (6, 7), and  $Co/Al_2O_3$ catalysts (8). In general, the zeolite-supported catalysts are more effective at lower temperatures and lower oxygen partial pressures, whereas the corresponding aluminasupported catalysts are more effective at higher temperatures and higher oxygen partial pressures.

Previously, it has been suggested that the competitive factor can be used to compare the effectiveness of lean NO<sub>x</sub> catalysts (9), which is defined as the ratio of the moles of



Here, we report the catalytic properties of highly active  $Sn/\gamma - Al_2O_3$  for lean  $NO_x$  reduction. The  $\gamma - Al_2O_3$ , prepared using a complexing agent, has been demonstrated to be unusual in its capacity to disperse cobalt oxide (8). The results of our study on the effect of Sn loading and the dependence of the N2 yield on the partial pressures of oxygen, water, and  $SO_2$  in the feed are reported.

γ-Al<sub>2</sub>O<sub>3</sub> was prepared from the hydrolysis of Al isopropoxide in 2-methylpentane-2,4-diol following the procedure of Maeda et al. (15). The Sn/Al<sub>2</sub>O<sub>3</sub> catalysts were prepared by incipient wetness impregnating with an amount of ethanol solution of SnCl<sub>2</sub> (Aldrich, 99.99+%) equal to the pore volume  $(1.4 \text{ cm}^3 \text{ g}^{-1})$ . The concentrations of SnCl<sub>2</sub> in the solution were adjusted so as to yield the desired Sn loadings in the final catalysts. The samples were then dried



<sup>&</sup>lt;sup>1</sup> On leave from Korea Electric Power Research Institute.

<sup>&</sup>lt;sup>2</sup> Corresponding author.

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TABLE 1

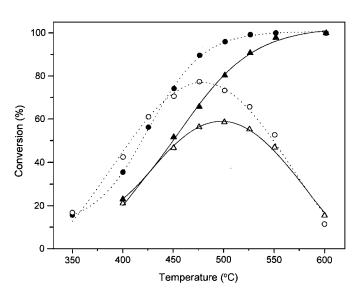
Sample	Sn content (wt%)	Surface area (m² g <sup>-1</sup> )	Competitiveness factor (temp. °C)
Al <sub>2</sub> O <sub>3</sub>	0	242	
Sn1	1.3	232	8.6 (525)
Sn5	4.6	224	10.1 (475)
Sn10	8.1	213	8.2 (500)
Sn15	14	184	9.4 (475)

in an air oven at  $100^{\circ}$ C overnight, and then calcined at  $500^{\circ}$ C for 4 h and then at  $800^{\circ}$ C for 2 h. The BET surface areas of the samples and their Sn contents are shown in Table 1.

X-ray diffraction of the samples showed diffraction peaks of only  $\gamma\text{-}Al_2O_3$  for sample Sn1, and additional peaks due to SnO\_2 also for samples Sn5, Sn10, and Sn15. The same diffraction pattern was obtained for sample Sn10 after reaction, except that the SnO\_2 peaks were slightly broader. From the areas of the SnO\_2 peaks, it was estimated that about  $40\pm10\%$  of the Sn in Sn5, and  $100\pm15\%$  of the Sn in Sn10 and Sn15 samples were in the crystalline form. Interestingly, the peak widths for the Sn5 and Sn10 samples were narrow, close to the instrument line width, but that for Sn15 was considerably wider. This suggests the there is a significantly higher degree of disorder in the SnO\_2 crystallites in Sn15. This will be described in detail in a later publication (16).

NO reduction was carried out in a flow of 5 to 15%  $O_2$ , 0 to 10%  $H_2O$ , 0.1% NO, and 0.1% propene, with the balance being He. Unless noted, the total flow rate was 200 ml/min, and 0.2 g of catalyst was used, which corresponded to a space velocity of 30,000  $h^{-1}$ . The catalysts were pretreated in the reaction feed at  $600^{\circ}$ C for 2 h before the data were collected. The reaction products were analyzed by gas chromatography as described earlier (8). NO conversions was determined by the  $N_2$  produced. No  $N_2O$  was detected. Thus, the  $N_2$  yield equaled the NO conversion.

Figure 1 shows the NO and propene conversions using 15% O<sub>2</sub> and 10% H<sub>2</sub>O as a function of temperature for a Sn10 catalyst at two space velocities  $(15,000 \text{ and } 30,000 \text{ h}^{-1})$ . As expected, conversions of NO to  $N_2$  at the lower space velocity were higher at lower temperatures. Significant conversions could be detected above 350°C, even in the presence of 15% O<sub>2</sub> and 10% H<sub>2</sub>O. The N<sub>2</sub> yield versus temperature profile was volcano-shaped, similar to the behavior of other lean NO<sub>x</sub> catalysts. At a space velocity of  $30,000 \,\mathrm{h^{-1}}$ , a maximum N<sub>2</sub> yield of about 58% was obtained at 500°C, which corresponded to an integral reaction rate of  $2.9 \times 10^{-2}$  mol NO/min-mol Sn. The maximum yield for 15,000 h<sup>-1</sup> space velocity was 77% for an integral rate of  $1.9 \times 10^{-2}$  mol NO/min-mol Sn. In order to illustrate the effect of different variables more clearly, a space velocity of 30,000 h<sup>-1</sup> was chosen as the standard test condition.



**FIG. 1.** The effect of space velocity on the NO reduction activity over Sn10 catalyst (0.1% NO, 0.1%  $C_3H_6$ , 15%  $O_2$ , 10%  $H_2O$ ). Total flow 100 cc/min (O:  $N_2$  yield,  $\blacksquare$ :  $C_3H_6$  conversion) or 200 cc/min ( $\triangle$ :  $N_2$  yield,  $\blacksquare$ :  $C_3H_6$  conversion).

The effect of Sn loading is illustrated in Fig. 2. The addition of Sn to  $\gamma$ -Al<sub>2</sub>O<sub>3</sub> enhanced the NO reduction activity significantly at temperatures below 525°C (Fig. 2a). The N<sub>2</sub> yield increased sharply from 1 wt% to 5 wt% Sn loading, but beyond that no further improvement was observed. In fact, when the Sn loading reached 15 wt%, a slight decline in NO conversion was observed. The integral reaction rates at the point of maximum NO conversion for the various catalysts are shown in Table 2. The apparently high activity of sample Sn1, however, is misleading because these rates have not been corrected for the SnO<sub>x</sub> dispersion. A similar trend in propene oxidation activity with Sn loading existed (Fig. 2b). Thus, the competitiveness factors at point of maximum NO conversion were not very different for catalysts with different Sn loadings, being around 9% (Table 1).

The dependence of NO conversion on the partial pressure of  $O_2$  is shown in Fig. 3. Below 475°C, both the  $N_2$  yield (Fig. 3a) and the hydrocarbon conversion (Fig. 3b) increased slightly with increasing  $O_2$  partial pressure. This

TABLE 2
Integral NO Conversion Rates and the Corresponding
Temperatures

Sample	Maximum NO conv. %	Temp. °C	Integral rate, 10 <sup>-2</sup> mol NO/min-mol Sn
Sn1	57	530	28
Sn5	59	480	5.8
Sn10	58	500	2.9
Sn15	47	475	1.5

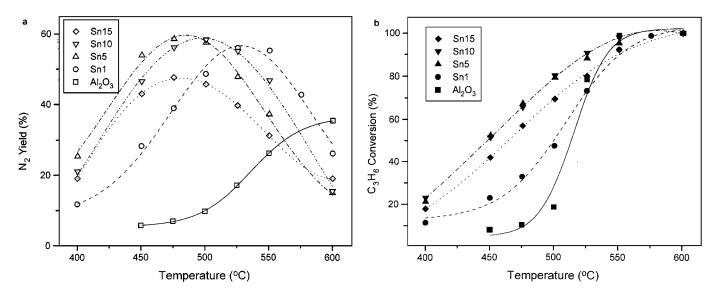


FIG. 2. The effect of Sn loading on the NO reduction activity over Sn/Al<sub>2</sub>O<sub>3</sub> Catalysts (0.1% NO, 0.1%  $C_3H_6$ , 15% O<sub>2</sub>, 10%  $H_2O$ , total flow 200 cc/min): (a) N<sub>2</sub> yield; (b)  $C_3H_6$  conversion.

observation differed somewhat from those of Ref. (12), where it was reported that the NO conversion, but not the alkene conversion, decreased slowly beyond the optimal partial pressure of 4% O<sub>2</sub>. The high N<sub>2</sub> yield at a high O<sub>2</sub> partial pressure is unusual among lean NO<sub>x</sub> reduction catalysts, where the active component is a reducible metal cation.

The effect of water partial pressure is shown in Fig. 4.  $H_2O$  suppressed NO conversion below 500°C, and the inhibitory effect was more severe at lower temperatures (Fig. 4a). Nonetheless, at 450°C, a  $N_2$  yield of 46% was still obtained with 10% water. Propene conversion was similarly sup-

pressed (Fig. 4b), and it appears that there is no preferential inhibition of the combustion sites as the competitiveness factors did not change significantly with the water partial pressure. This result differs from the work of Miyadera *et al.* (13), where they reported an increase in the competitiveness factor in the presence of water.

Finally, the effect of  $SO_2$  was examined and the results are shown in Fig. 5. Addition of 30 ppm  $SO_2$  in the feed did not suppress the NO reduction activity at  $475^{\circ}$ C until after about 4 h on stream. The NO conversion declined slowly for 10 to 15 h from 58% to 40%, when the activity appeared to be stabilized. The conversion recovered slowly upon

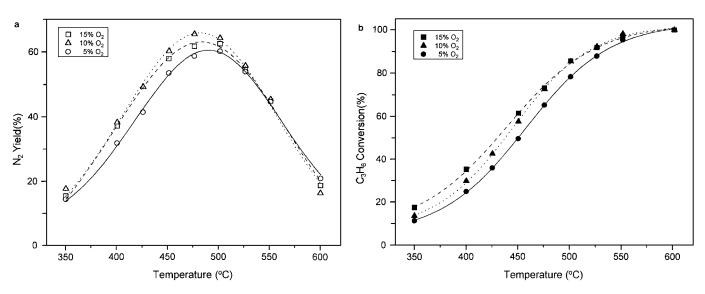


FIG. 3. The effect of  $O_2$  partial pressure on the NO reduction activity over Sn10 sample (0.1% NO, 0.1%  $C_3H_6$ , 5–15%  $O_2$ , 4%  $H_2O$ , total flow 200 cc/min): (a)  $N_2$  yield; (b)  $C_3H_6$  conversion.

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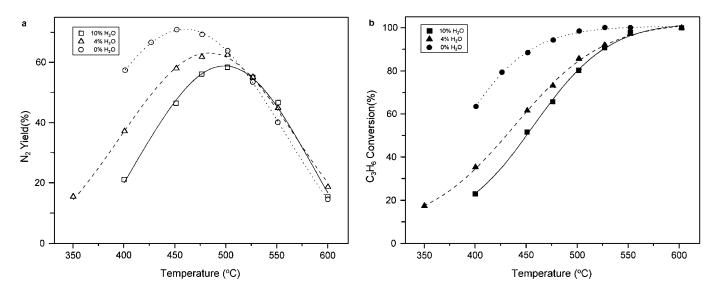
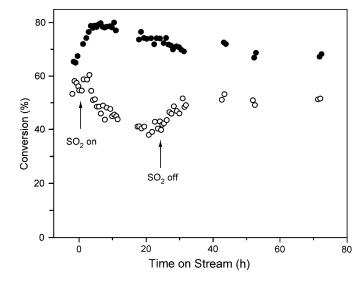


FIG. 4. The effect of  $H_2O$  partial pressure on the NO reduction activity over Sn10 catalyst (0.1% NO, 0.1%  $C_3H_6$ , 15%  $O_2$ , 0–10%  $H_2O$ , total flow 200 cc/min): (a)  $N_2$  yield; (b)  $C_3H_6$  conversion.

removal of  $SO_2$  from the feed to 52%. In another experiment in which the activity of the catalyst between 450 and 550°C was examined, the conversion at 475°C recovered to over 60%. In addition, when  $SO_2$  was reintroduced, the conversion returned to 40%. Thus,  $SO_2$  is not a permanent poison for the Sn active sites. Instead, it is adsorbed quite strongly on  $Al_2O_3$ , which has a rather high sorption capacity, and the slow recovery of the activity was due to slow desorption of  $SO_2$  from it. Without  $SO_2$ , the activity of the catalyst did not decrease after six days of experiments in the presence of 10%  $H_2O$ , and it might even increase slightly.



**FIG. 5.** The effect of  $SO_2$  on the NO reduction activity over Sn10 catalysts: O,  $N_2$  yield;  $\blacksquare$ ,  $C_3H_6$  conversion (0.1% NO, 0.1%  $C_3H_6$ , 15%  $O_2$ , 10%  $H_2O$ , 30 ppm  $SO_2$ , total flow 200 cc/min).

In summary, the data presented show that  $Sn/Al_2O_3$  are effective  $NO_x$  reduction catalysts. Although the nature of the active sites is not yet known at present, these catalysts showed stable, high activities above  $400^{\circ}$ C, even at high partial pressures of  $O_2$  and  $H_2O$ . This temperature range would be suitable for treatment of exhaust from heavy duty diesel engines. Although the activity was suppressed by  $SO_2$ , the effect was reversible. Together with other  $Al_2O_3$ -supported catalysts that have demonstrated high  $NO_x$  conversion ability, it appears probable that effective  $NO_x$  reduction catalysts can be prepared on alumina and perhaps other supports, in addition to zeolites, especially for high stability under harsh conditions of high temperatures and water partial pressures.

## ACKNOWLEDGMENTS

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